### General description
Trapezoidal threads are ideal for movement due to their flank profile. Application: Conversion of a rotary movement into a linear one. Sometimes: Conversion of a linear movement into a rotary one. Trapezoidal threads can also be used as easy-to-loosen fastener.

### Thread profile of the catalogue products
Metric DIN-ISO thread according to DIN 103, with 15° flank angle.

### Designation of a Trapezoidal thread spindle DIN 103
DIN-number, abbreviation for trapezoidal thread, outside diameter x lead x length
For example: Spindle DIN 103 Tr. 12 x 3 x 1000mm.

### Production method
Practically all of the spindles in the catalogue models are rolled. Thread rolling is the most economical production method for series production. Due to the chipless shaping, rolled threaded spindles feature a number of positive characteristics: Higher tensile strength, higher resistance to wear, higher fatigue strength under reversed bending, burnished thread flanks, precise profile, unsevered grain structure and higher resistance to corrosion. During thread rolling a groove forms at the outside diameter. This groove guarantees accuracy and cylindricity of the thread. It has no influence on the functioning of the threaded spindle, as the thread bears its load at the flanks. The threads of the nuts are cut.

### Lubrication
Running without lubricant is not allowed. For grease lubrication, normal roller bearing grease is recommended. The lubricant consumption depends on the condition of use.

### Catalogue Spindles page 446 - 448

<table>
<thead>
<tr>
<th>Specification</th>
<th>Steel C15</th>
<th>Stainless 1.4305</th>
<th>Page</th>
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</thead>
<tbody>
<tr>
<td>Single thread right and left</td>
<td>Tr. 10 x 3 to Tr. 70 x 10</td>
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<tr>
<td>Double thread, right hand</td>
<td>Tr. 10 x 3 to Tr. 50 x 8</td>
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<td>Tr. 12 x 6P3 to Tr. 40 x 14P7</td>
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</tr>
<tr>
<td></td>
<td>Tr. 12 x 6P3 to Tr. 40 x 14P7</td>
<td>Page 448</td>
<td></td>
</tr>
</tbody>
</table>

Stock lengths: 1000mm, 1500mm, 2000mm, 3000mm.
Other lengths and materials as well as customised models on request.

### Stock Spindles page 451 - 450

- **Round nuts or hexagon nuts made from steel C35Pb and stainless steel 1.4305.**
  For clamping, manual adjustment and as a fastening nut. Not suitable for drive systems. Trapezoidal nuts from steel or stainless steel tend to stick (seizure) on spindles from steel or stainless. They must be well lubricated and are movable only for short time at low speed.

- **Round nuts or round flange nuts made from red brass Rg7.**
  For drive systems at low and medium speed and operating times under 20%. Good dry running properties in situations with insufficient lubrication. In combination with a stainless spindle the drive becomes corrosion resistant.

- **Round flange nuts made from cast iron GG25.**
  As for round flange nut made from red brass but only limited dry-running capabilities and not corrosion proof.

- **Round nuts made from plastic PA6.6 with MoS2.**
  For low-noise drive systems. Maximum permissible peripheral speed \( v_{\text{max}} = 0.5 \text{ m/sec.} \) at low load. Good dry-running properties.

Spindle and nut components are manufactured in accordance with DIN 103. Zero backlash (adjustable) can only be achieved with a two-part nut or two counteracting nuts. Spindles and spindle nuts available from drawing on request.

### Ball Screw Drives page 454

### Bearing Units for Spindels page 414
The required output torque at the spindle can be derived from the axial load, the lead of the spindle and the efficiency of threaded spindle drive and mounting. At short acceleration times and high speeds, the acceleration torque, and with sliding guide the breakaway torque also have to be considered.

**Calculation method:**
1) Determining the lead angle using α from book of tables or DIN sheet or through calculation.
2) Determining the friction coefficient µ using a table.
3) Calculating the effective angle of friction p'.
4) Calculating the degree of efficiency η.
5) Calculating the torque Md.

**Important:** About 10% should be added to the end result to make up for losses due to bearing situation. Additional friction due to linear guides and possible rotational forces have to be considered by adding a respective allowance. This can also be done when calculating the input power.

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**Legend**

- α (alpha) is the lead angle of the thread.
- η (eta) is the degree of efficiency regarding the conversion of rotary into linear motion.
- η' is the degree of efficiency regarding the conversion of linear into rotary motion.
- µ (mu) is the friction coefficient.
- π (pi) is \( \approx 3.14 \).
- \( \tan \alpha = \frac{p}{d_2 \cdot \pi} \)
- \( \tan p' = \mu \cdot 1.07 \)
- \( \eta = \frac{\tan \alpha}{\tan (\alpha + p')} \)
- \( M_d = \frac{F \cdot P \cdot \eta'}{2000 \cdot \pi \cdot \eta} \)

---

**Self-locking Capacity of Trapezoidal Spindle Drives**

The self-locking capacity is linked to the friction coefficient (determined by the material match spindle/nut, surface quality, lubrication) and to the lead angle. If the lead angle is smaller than the angle of friction, the spindle drive is self-locking.

We need to distinguish between static and dynamic self-locking capacity. With static self-locking capacity a motionless nut remains steadfast, as long as it is not set in motion by other influences. With dynamic self-locking capacity a moving nut comes to a stop, when it is no longer driven.

In theory all listed single-thread spindle drives - except for plastic nuts - are self locking, as the lead angle is smaller than the angle of friction. A small vibration may, however be enough to set the nut moving. The only dynamic self-locking drive is size 70 x 10, as only here the lead angle is small enough (friction coefficient 0.05 \( \approx 2.86^\circ \)).

**Attention:** The above statements are only valid under the assumption that the friction coefficients listed in the catalogue are really fitting. In practice surface properties and the type of lubrication and lubricant used may cause deviation from the original value. To be on the safe side, a locking device (clamping device) should be fitted. In connection with plastic nuts, none of the spindle drives listed are self-locking.

**Required Driving Power of a Spindle Drive**

The power (in kW) can be derived from the driving torque \( M_d \) and the spindle speed \( n \) (in min\(^{-1}\)):

\[ P = \frac{M_d \cdot n}{2000 \cdot \pi} \]

**Important:** In order to allow for losses caused by the bearing and other frictional losses and the power required for rotary acceleration, the power selected for the drive should be 60 to 100% above the calculated figure.
Basis for the Calculation of Trapezoidal-Threaded Spindle Drives

Critical Speed of Trapezoidal-Thread Spindles

With thin, fast running spindles there is a danger that resonant bending vibration occurs. The method described below helps to determine the resonant frequency provided a rigid enough installation. Speeds close to the critical speed also immensely increase the risk of lateral buckling - the critical speed must therefore always be considered when calculating the critical buckling length. (see following chapter “critical buckling force”)

\[
n_{perm.} = n_{kr} \cdot f_{kr} \cdot c_{kr}
\]

- \( n_{perm.} \) is the fastest permissible spindle speed in min\(^{-1}\).
- \( n_{kr} \) is the critical spindle speed in min\(^{-1}\) - corresponds to the natural bending vibrations of the spindle and leads to resonance occurrences.
- \( f_{kr} \) is a corrective factor, considering the spindle bearing. Precondition is a rigid enough installation of the spindle and a fixed bearing.

The following drawing shows 4 classic installation methods of \( f_{kr} \) for standard spindle bearings:

- \( f_{wr}=0,36 \)
- \( f_{wr}=1,47 \)
- \( f_{wr}=1 \)
- \( f_{wr}=2,23 \)

\( c_{kr} \) is a corrective factor, considering the influence of the critical buckling force. We would advise to first determine \( n_{kr} \), \( f_{kr} \) and to then to equate \( n_{perm} \) with the actual speed \( n \). This then leads to \( c_{kr} \) for \( n/(n_{kr} \cdot f_{kr}) \), and with these figures the diagram then renders \( c_{kr} \) the related maximum axial pressure load.

Critical Buckling Force of Trapezoidal-Threaded Spindles

With thin spindles under pressure load there is a risk that lateral buckling occurs. Before the permissible pressure load is determined, the safety factors of the mechanism have to be considered.

\[
F_{zul.} = F_{k} \cdot f_{k} \cdot c_{k}
\]

- \( F_{perm.} \) is the strongest permissible axial force (pressure load) on the spindle in kN.
- \( F_{k} \) is the critical buckling force in kN in connection with the free length \( L \).
- \( f_{k} \) is a corrective factor, considering the spindle bearing. Precondition is a rigid enough installation of the spindle and a fixed bearing. The following table shows classic installation methods of \( f_{k} \) for standard spindle ends.

\[
c_{k} \]

is a corrective factor, considering the influence of the critical speed.

\[
c_{kr} \]

is here calculated as follows:

\[
c_{kr} = \frac{n}{n_{kr} \cdot f_{kr}}
\]

- \( n \) is effective spindle speed in min\(^{-1}\).
- \( n_{kr} \) is the critical spindle speed in min\(^{-1}\) according to the diagramme above.
- \( f_{kr} \) is the corrective factor of the critical spindle speed, under of the spindle bearing method. Values for \( f_{k} \) see above.
Basis for the Calculation of Trapezoidal-Threaded Spindles

Load Capacity

The load capacity for slide pairings usually depends on the material used, the surface properties, intake condition, lubrication conditions and gliding speed, on the temperature and thus on the duty cycle and possibilities for heat dissipation as well as the type of load (constant, fluctuating, alternating, shocks...).

The diagrams below allow an assessment of the permissible axial load in connection with the speed of trapezoidal-threaded nuts on rolled trapezoidal-threaded spindles at normal operating conditions.

Load table for nuts made from steel C35 see page 445.

Regarding the Operating Times

Especially single-thread, trapezoidal-threaded spindle drives, due to their low degree of efficiency, convert most of the input power of the shaft into heat, which is first absorbed by spindle and then has to be dissipated. At low power and short operating times the natural dissipation and radiation of heat is usually sufficient. With continuous operation quite substantial cooling capacities might be required. As a thermodynamic calculation of these difficulties is usually too complex or even impossible, already existing comparative calculations are often the only source of information.

Round nuts made from red brass Rg7

Round nuts made from plastic

Round flange nuts made from cast iron GG25

Round flange nuts made from red brass Rg7

Approx. 80% of the axial force in kN are permissible for double-threaded nuts.
## Material Properties

This plastic is a low-maintenance material for bearings. Compared to other plastics it has a much higher wear resistance. The spec. surface pressure is 35 N/mm² at 23°C/50% RH. Threaded nuts made from plastic are more resistant against loads caused by impacts or shocks than red brass and grey cast iron-nuts. The material is also quieter than red brass and grey cast iron and increases the service life.

### Properties

<table>
<thead>
<tr>
<th>Property</th>
<th>Unit of Measurement</th>
<th>Plastic PA6.6 with MoS²</th>
</tr>
</thead>
<tbody>
<tr>
<td>Tensile Strength</td>
<td>N/mm²</td>
<td>90 (82)</td>
</tr>
<tr>
<td>Elongation at Break</td>
<td>%</td>
<td>20 (70)</td>
</tr>
<tr>
<td>Flexural Modus</td>
<td>N/mm²</td>
<td>3600 (1500)</td>
</tr>
<tr>
<td>Compressive Strength at 1% Deformation</td>
<td>N/mm²</td>
<td>37</td>
</tr>
<tr>
<td>Izod Impact, Notched</td>
<td>kJ/m²</td>
<td>3.35 (&gt;10)</td>
</tr>
<tr>
<td>Shore Hardness D</td>
<td>D</td>
<td>80 - 90</td>
</tr>
<tr>
<td>Coefficient of Linear Thermal Expansion</td>
<td>10⁻⁵°C</td>
<td>63</td>
</tr>
<tr>
<td>Thermal Conductivity</td>
<td>W/mk</td>
<td>0.21</td>
</tr>
<tr>
<td>Thermal Compr. Strength 0.46 N/mm² °C</td>
<td>204 - 254</td>
<td></td>
</tr>
<tr>
<td>Melting Point</td>
<td>°C</td>
<td>260</td>
</tr>
<tr>
<td>Resistivity</td>
<td>Ω cm</td>
<td>&gt;10¹³ (10¹²)</td>
</tr>
<tr>
<td>Dielectric Constant</td>
<td>-</td>
<td>3.5 (5.1)</td>
</tr>
<tr>
<td>Dissipation Factor</td>
<td>-</td>
<td>0.03 (0.2)</td>
</tr>
<tr>
<td>Water Absorption 24 hours</td>
<td>%</td>
<td>0.5 - 1.3</td>
</tr>
<tr>
<td>Water Absorption max.</td>
<td>%</td>
<td>6 - 8</td>
</tr>
</tbody>
</table>

Figures are valid for a water content below 0.2%, Figures in ( ) at standard climate 23°C/50% RH. Chemically resistant against all solutions, lubricants, hydrocarbons, ketones, aqueous solutions and alkali solutions pH5-pH11. Chemically unstable against phenols, cresols, formic acid, concentrated mineral acids and alkali, oxidisers including halogens.

## Wear Properties

Common constructions (threaded spindle made from steel, nut made from grey cast iron or bronze) lead to wear of the threaded spindle and the nut. A threaded nut made from plastic does not affect the spindle, i.e. if unexpected wear occurs, only the nut has to be changed. In the pairing steel/plastic there is generally no hardening of the spindle required.

### Fixing Plastic Nuts

The plastic nut can be pressed into the housing with a slight over-size of 0.1 - 0.2 mm. It can be secured against turning and displacement with any of the common locking elements used in machine building, or with a flange attached to the face side.

**Attention:** The over-size used for pressing the nut in passes on 1 : 1 to the inner diameter which reduces the clearance.

### Note

For systems with relatively high loads or extreme operating conditions we would advise you to contact us.

## Maintenance

The nuts only need to be lubricated on the first mounting, after that they are maintenance free. In order to prolong the service life of the nuts, they can be relubricated, if required. Any fat not containing molybdenum sulphide (Molykote) can be used.

### Tolerances

Other than for the rest of the trapezoidal-threaded nuts, the flank clearance is kept at the upper tolerance limit, as the plastic expands when heating up.

## Load Table for Single-Thread Steel Nuts in kN Static (without Safety Margin)

<table>
<thead>
<tr>
<th>Trapezoidal Thread Ø x Lead at h= 1.5 x d mm</th>
<th>Load Capacity at h= 1.5 x d kN</th>
<th>Length at h= 2 x d mm</th>
<th>Load Capacity at h= 2 x d kN</th>
</tr>
</thead>
<tbody>
<tr>
<td>10 x 3</td>
<td>15</td>
<td>3.6</td>
<td>20</td>
</tr>
<tr>
<td>12 x 3</td>
<td>18</td>
<td>6.3</td>
<td>24</td>
</tr>
<tr>
<td>14 x 4</td>
<td>21</td>
<td>6.9</td>
<td>28</td>
</tr>
<tr>
<td>16 x 4</td>
<td>24</td>
<td>9.2</td>
<td>32</td>
</tr>
<tr>
<td>18 x 4</td>
<td>27</td>
<td>11.8</td>
<td>36</td>
</tr>
<tr>
<td>20 x 4</td>
<td>30</td>
<td>14.8</td>
<td>40</td>
</tr>
<tr>
<td>24 x 5</td>
<td>36</td>
<td>21.2</td>
<td>48</td>
</tr>
<tr>
<td>28 x 5</td>
<td>42</td>
<td>29.2</td>
<td>56</td>
</tr>
<tr>
<td>30 x 6</td>
<td>45</td>
<td>33.4</td>
<td>60</td>
</tr>
<tr>
<td>32 x 6</td>
<td>48</td>
<td>35.8</td>
<td>64</td>
</tr>
<tr>
<td>36 x 6</td>
<td>54</td>
<td>48.9</td>
<td>72</td>
</tr>
<tr>
<td>40 x 7</td>
<td>60</td>
<td>60.2</td>
<td>80</td>
</tr>
<tr>
<td>44 x 7</td>
<td>66</td>
<td>73.1</td>
<td>88</td>
</tr>
<tr>
<td>48 x 8</td>
<td>72</td>
<td>87.2</td>
<td>96</td>
</tr>
<tr>
<td>50 x 8</td>
<td>75</td>
<td>94.9</td>
<td>100</td>
</tr>
<tr>
<td>52 x 8</td>
<td>78</td>
<td>102.9</td>
<td>104</td>
</tr>
<tr>
<td>60 x 9</td>
<td>90</td>
<td>137.3</td>
<td>120</td>
</tr>
<tr>
<td>70 x 10</td>
<td>105</td>
<td>213.3</td>
<td>-</td>
</tr>
</tbody>
</table>

**Reworking within 24h-service possible. Custom made parts on request.**